

Ch3 Part 3

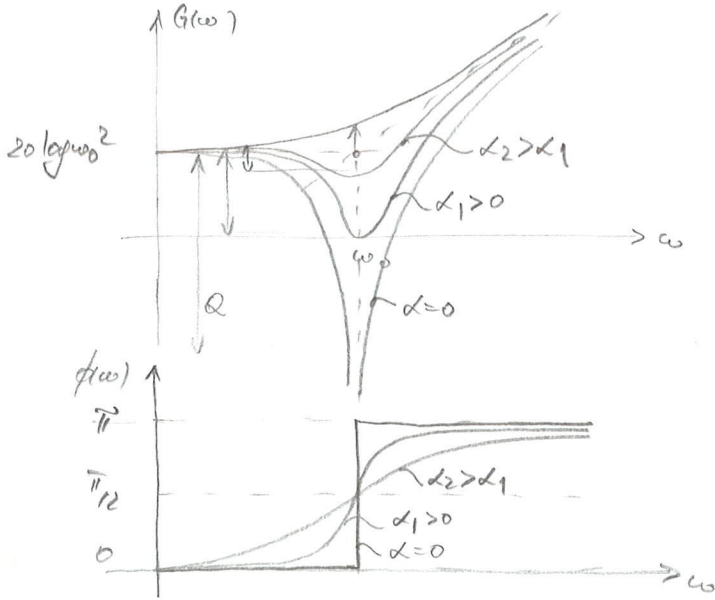
$$H(s) = s^2 + 2\alpha s + \omega_0^2$$

$$H(j\omega) = (\omega_0^2 - \omega^2) + j2\alpha\omega = \text{Re}(H(j\omega)) + j\text{Im}(H(j\omega))$$

asymptotes

$$\text{Gain: } G(\omega) = |H(j\omega)|_{dB} = 20 \log \sqrt{(\omega_0^2 - \omega^2)^2 + 4\alpha^2\omega^2} = \begin{cases} 20 \cdot \log \omega_0^2 & , \omega \rightarrow 0, \omega \ll \omega_0 \\ 20 \cdot \log \omega^2 & , \omega \rightarrow \infty, \omega \gg \omega_0 \end{cases}$$

$$\text{Phase: } \phi(\omega) = \arg(H(j\omega)) = \arctan \frac{2\alpha\omega}{\omega_0^2 - \omega^2} = \begin{cases} 0 & , \omega \rightarrow 0, \omega \ll \omega_0 \\ \frac{\pi}{2} & , \omega = \omega_0 \\ \pi - \arctan \frac{2\alpha\omega}{\omega^2} \rightarrow \pi & , \omega \gg \omega_0, \omega \rightarrow \infty \end{cases}$$



$$\text{Quality factor } Q = \frac{\omega_0}{2\alpha}$$

$$Q = \frac{|H(0)|}{|H(\omega_0)|} = \frac{\omega_0^2}{2\alpha\omega_0} = \frac{\omega_0}{2\alpha}$$

Teoreme constanten de timp?

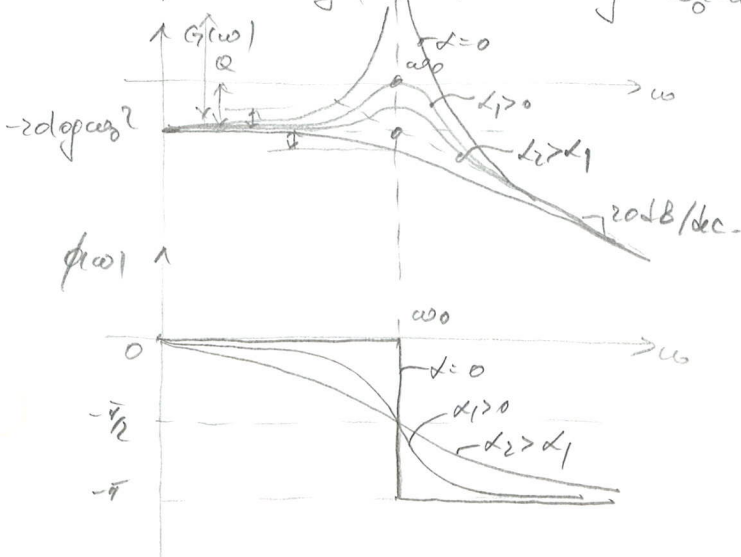
Rep in circuit with pure C & L
 nu tin prop. of zero or pole!

Known as "open-circuit time constant" or "zero-value time constant technique"

$$H(s) = \frac{1}{s^2 + 2\alpha s + \omega_0^2} \Rightarrow H(j\omega) = \frac{1}{(\omega_0^2 - \omega^2) + j2\alpha\omega}$$

$$\text{Gain: } G(\omega) = -20 \log \sqrt{(\omega_0^2 - \omega^2)^2 + 4\alpha^2\omega^2} = \begin{cases} -20 \log \omega_0^2 & , \omega \rightarrow 0, \omega \ll \omega_0 \\ -20 \log \omega^2 & , \omega \rightarrow \infty, \omega \gg \omega_0 \end{cases}$$

$$\text{Phase: } \phi(\omega) = -\arg(H(j\omega)) = -\arctan \frac{2\alpha\omega}{\omega_0^2 - \omega^2} = \begin{cases} 0 & , \omega \rightarrow 0 \\ -\frac{\pi}{2} & , \omega = \omega_0 \\ -\pi & , \omega \rightarrow \infty \end{cases}$$



$$\text{Quality factor } Q = \frac{\omega_0}{2\alpha}$$

$$Q = \frac{|H(\omega_0)|}{|H(0)|} = \frac{\frac{1}{2\alpha\omega_0}}{\frac{1}{\omega_0^2}} = \frac{\omega_0^2}{2\alpha\omega_0} = \frac{\omega_0}{2\alpha}$$

obs: The textbook uses this notation:

$$H(s) = \frac{N(s)}{\left(\frac{s}{\omega_0}\right)^2 + 2\zeta \cdot \left(\frac{s}{\omega_0}\right) + 1} = \frac{\overset{\text{const}}{\omega_0^2} \cdot N(s)}{s^2 + 2\zeta \cdot \omega_0 \cdot s + \omega_0^2}$$

with $\omega = \omega_0$ notation our discussion so far is easier to understand

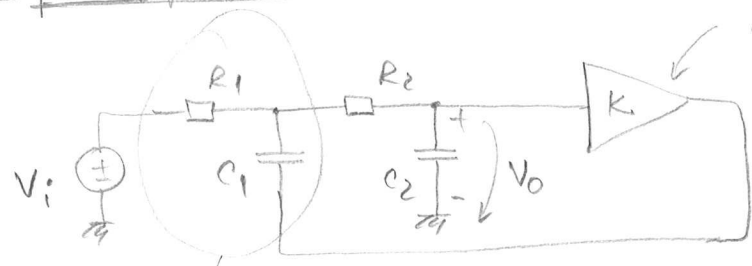
Depending on the $N(s)$, we can have various filters:

- Low-pass response	LP	$H_{LP}(j\omega) = \frac{1}{1 - \left(\frac{\omega}{\omega_0}\right)^2 + j \cdot \frac{\omega}{\omega_0} \cdot \frac{1}{Q}}$
- High-pass	HP	$H_{HP}(j\omega) = \frac{-\left(\frac{\omega}{\omega_0}\right)^2}{1 - \left(\frac{\omega}{\omega_0}\right)^2 + j \cdot \frac{\omega}{\omega_0} \cdot \frac{1}{Q}}$
- Band-pass	BP	$H_{BP}(j\omega) = \frac{j \cdot \frac{\omega}{\omega_0} \cdot \frac{1}{Q}}{1 - \left(\frac{\omega}{\omega_0}\right)^2 + j \cdot \frac{\omega}{\omega_0} \cdot \frac{1}{Q}}$
- Notch	N	
- All-pass	AP	$H_{AP}(j\omega) = \frac{1 - \left(\frac{\omega}{\omega_0}\right)^2}{1 - \left(\frac{\omega}{\omega_0}\right)^2 + j \cdot \frac{\omega}{\omega_0} \cdot \frac{1}{Q}}$

These are standard forms!

$$H_{LP} + H_{HP} = 1 - H_{BP} = H_N$$

3.5 KRC filters



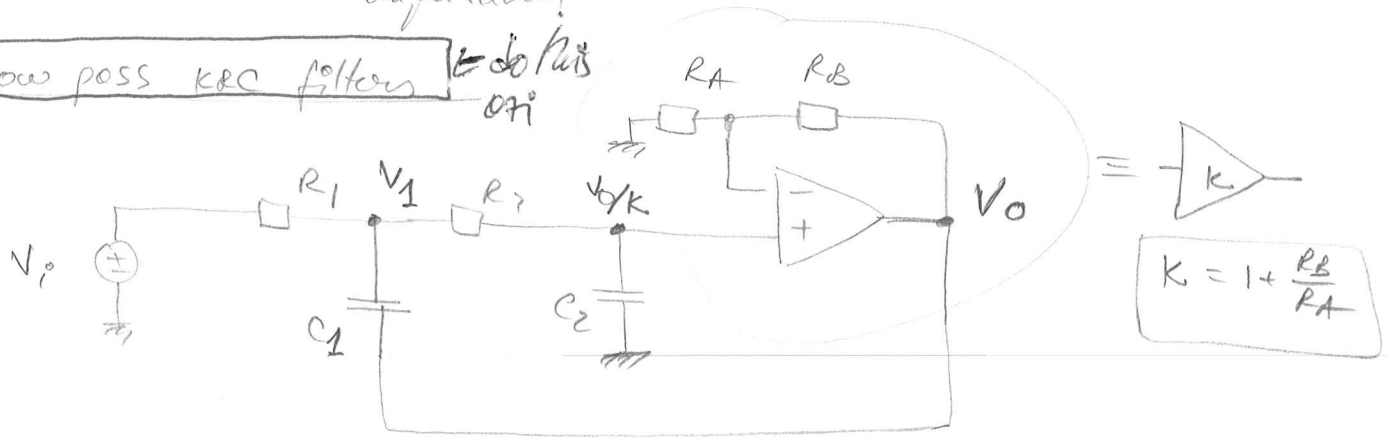
controls the magnitude at ω_0
 $\omega_0 = \sqrt{\omega_1 \omega_2}$
 it increases Q!

$$H(s) = \frac{1}{sC_1} \cdot \frac{1}{R_2 + \frac{1}{sC_2}} = \frac{1}{sRC_1 + 1} \xrightarrow{s \rightarrow j\omega} \frac{1}{j\omega RC_1 + 1} \xrightarrow{\omega \rightarrow \omega_0} \frac{1}{j \frac{\omega}{\omega_0}}$$

$$H(s) \xrightarrow{\omega \rightarrow \infty} \frac{1}{j \frac{\omega}{\omega_1}} \cdot \frac{1}{j \frac{\omega}{\omega_2}} = \frac{1}{(\omega/\omega_0)^2}, \quad \omega_0 = \sqrt{\omega_1 \omega_2}$$

Here $\frac{\omega}{\omega_0} \rightarrow 1$ the positive feedback realized by K will control the amplitude!

Low pass KRC filters



$$\left\{ \begin{array}{l} V_o = K \cdot \frac{1}{sR_2C_2 + 1} \cdot V_1 \\ \text{KCL: } \frac{V_i - V_1}{R_1} + \frac{V_o/K - V_1}{R_2} + \frac{V_o - V_1}{\frac{1}{sC_1}} \end{array} \right. \Rightarrow$$

$$\Rightarrow H(s) = \frac{V_o}{V_i} = \frac{K}{R_1 R_2 C_2 s^2 + [(1-K)R_1 C_1 + R_1 C_2 + R_2 C_2] s + 1}$$

Use standard form: $s \rightarrow j\omega$, $H(j\omega) = H_{OLP} H_{LFP}(j\omega)$

where: $H_{OLP} = K$

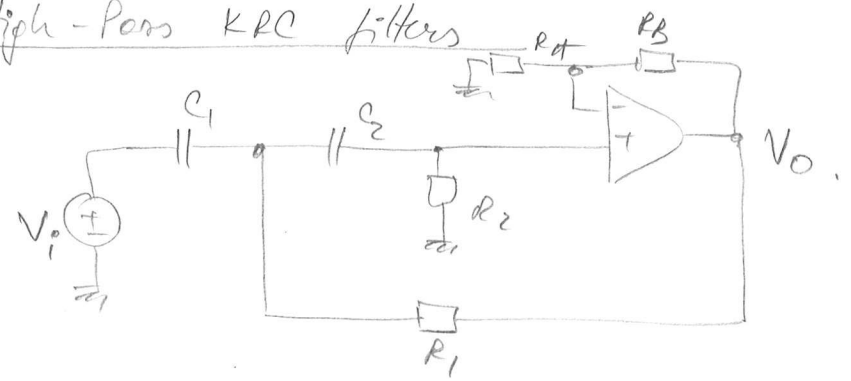
$$\omega_0 = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}}$$

$$Q = \frac{1}{(1-K)\sqrt{R_1 C_1 / R_2 C_2} + \sqrt{R_2 C_2 / R_1 C_1} + \sqrt{R_2 C_2 / R_1 C_1}}$$

Use $\begin{cases} R_1 = R_2 = R \\ C_1 = C_2 = C \end{cases}$ commonly!

$K = 3 - \frac{1}{Q}$, design for $Q = 5$, $K = ?$

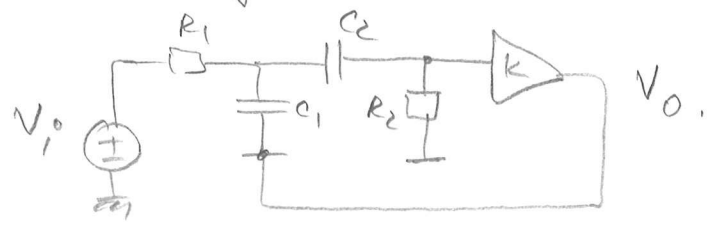
ⓑ High-Pass KRC filters



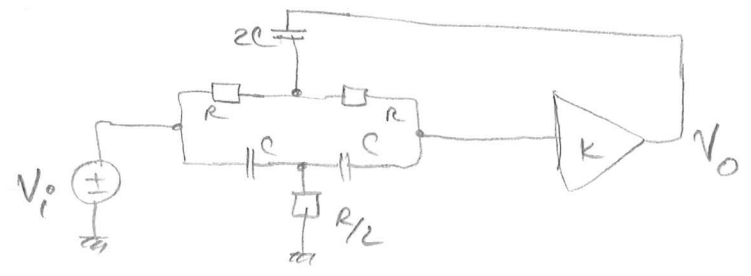
Resistor C's are swapped!

ⓒ Band-Pass KRC filter

How would you connect R_1, C_1, R_2, C_2 ?



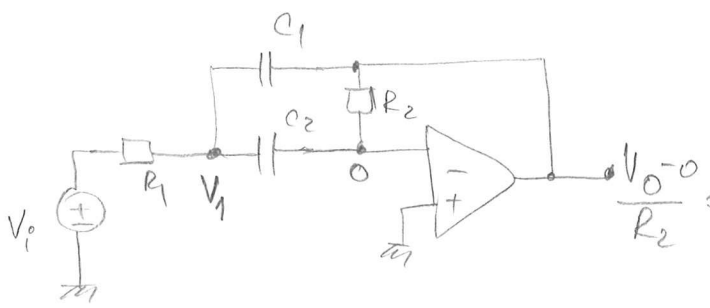
ⓓ Band-Reject KRC filter



3.6 Multiple-feedback filters

Utilize more than one feedback path!
Some of the most popular op amp filters.

(a) Band-Pass



$$\frac{V_0 - 0}{R_2} = - \frac{V_1 - 0}{\frac{1}{sC_1}} \Rightarrow V_0 = -sR_2C_2 \cdot V_1$$

$$\text{KCL: } \frac{V_1 - V_1}{R_1} + \frac{V_0 - V_1}{\frac{1}{sC_1}} + \frac{0 - V_1}{\frac{1}{sC_2}} = 0.$$

$$\Rightarrow \text{As } s \rightarrow j\omega \quad H(j\omega) = \frac{V_0}{V_1} = \frac{-j\omega R_2 C_2}{1 - \omega^2 R_1 C_1 R_2 C_2 + j\omega R_1 (C_1 + C_2)} \quad \boxed{\text{BP}}$$

Standard form:

$$H(j\omega) = H_{\text{BPF}} \cdot H_{\text{BP}}(j\omega)$$

where:

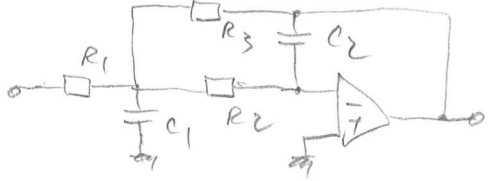
$$\omega_0 = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}}$$

$$Q = \frac{\sqrt{\frac{R_2}{R_1}}}{\sqrt{\frac{C_1}{C_2}} + \sqrt{\frac{C_2}{C_1}}}$$

$$H_{\text{BPF}} = - \frac{\frac{R_2}{R_1}}{1 + \frac{C_1}{C_2}}$$

(b) Low-Pass

How would you shuffle R_1, C_1, R_2, C_2 ?



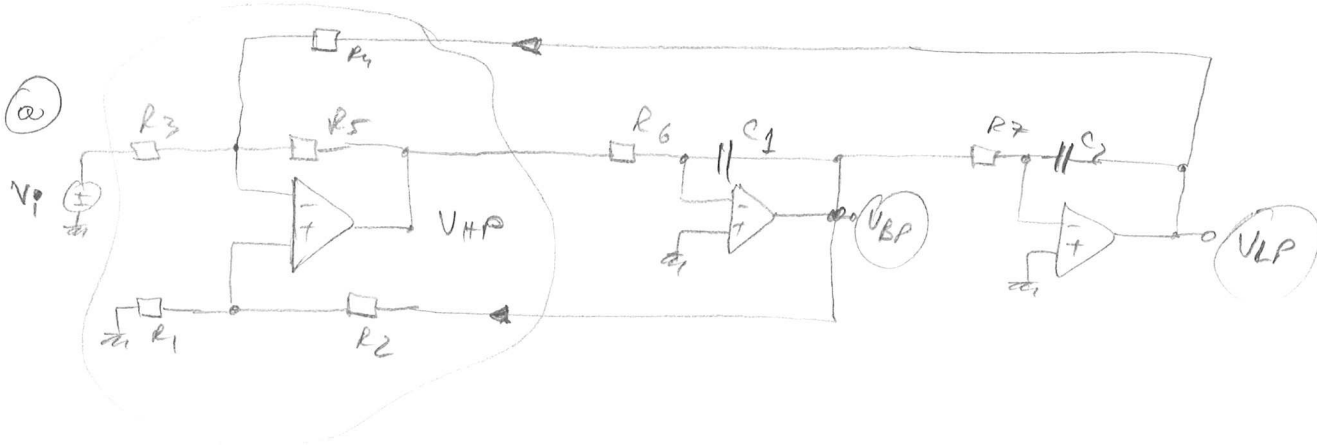
(c) Notch filters

(6)

3.7 (a) State variables (SV) Filters.

(b) Biquad filters

} use mode of drops.



(b) Biquad

(c) Notch filter