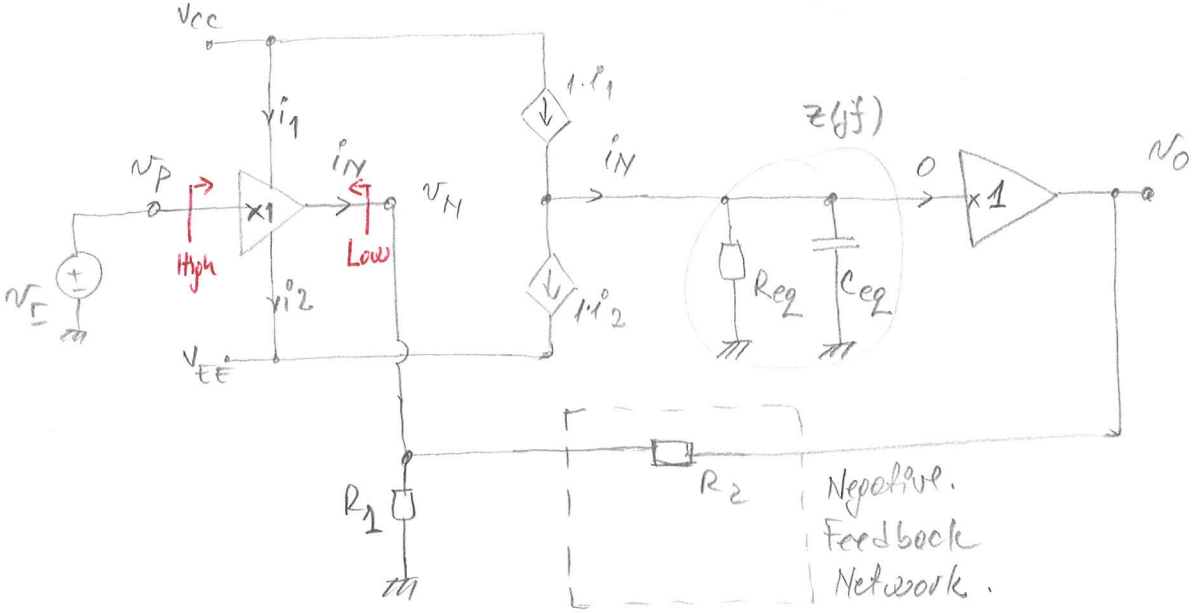


6.7. Current feedback amplifiers

current-mode operation = much faster.

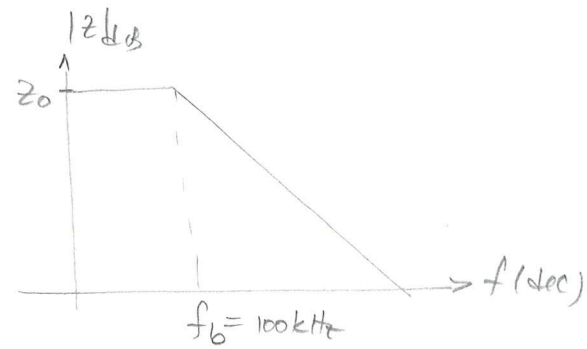


Obs: Auto application examples!

$i_N = i_1 - i_2$

(1) $V_O = Z(jf) \cdot I_N$
 ← by construction
 ↑ open-loop transimpedance gain.

(2) $Z(jf) = \frac{z_0}{1 - j \frac{f}{f_b}}$, $f_b = \frac{1}{2\pi R_{eq} C_{eq}}$

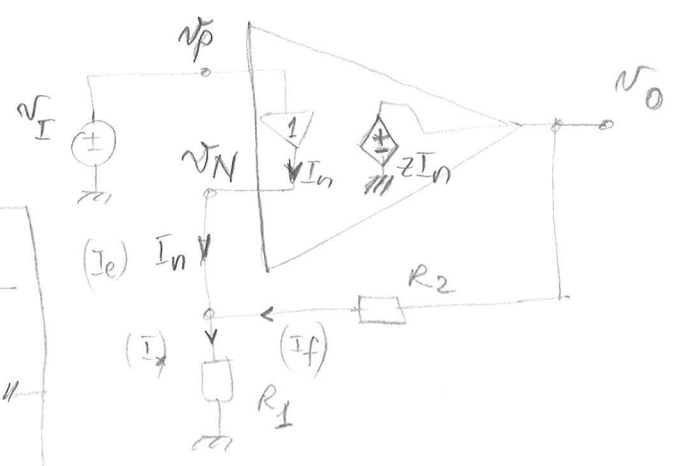


Closed-loop gain

superposition

(3) $I_N = \frac{V_i}{R_1 || R_2} - \frac{V_O}{R_2}$
 ← due to feedback

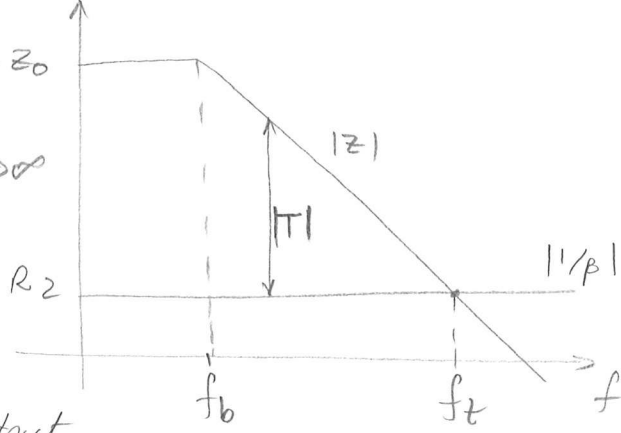
(1), (3) => $A(jf) = \frac{V_O}{V_i} = \left(1 + \frac{R_2}{R_1}\right) \frac{1}{1 + \frac{1}{T(jf)}}$
 where $T(jf) = Z(jf) \cdot \frac{1}{R_2} = Z(jf) \cdot \beta_g$



$T(jf) \triangleq$ loop gain $R_{eq} = z_0$

To maximize $T \Rightarrow$ increase $z(jf) \rightarrow \infty$

(1) $\Rightarrow I_n$ will be very small $\rightarrow 0$



\Rightarrow CFA will provide whatever output necessary to drive I_n to zero.

Conclusion:

		CFA	VFA
input voltage constraint	$V_n \rightarrow V_p$	by design	by neg. feedback
input current constraint	$I_p \rightarrow 0, I_n \rightarrow 0$	by negative feedback.	by design

We can apply these constraints during CFA-based circuits as well!

CFA Dynamics - Bandwidth

$$A(jf) = A_0 \times \frac{1}{1 + j f/f_t}$$

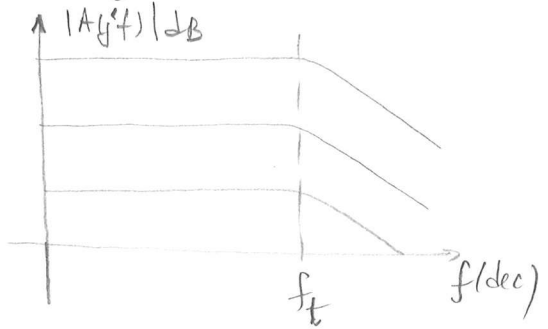
closed loop gain \rightarrow

$$\left(1 + \frac{R_2}{R_1}\right) \cdot \frac{1}{1 + j f/f_t}$$

$$f_t = \frac{1}{2\pi R_2 C_{eq}}$$

bandwidth, depends only on $R_2!$
100MHz typically

Use R_2 to set bandwidth and use R_1 to adjust $A_0!$



Transient response

$$V_I = V_{in} \cdot u(t) \Rightarrow i_N = \frac{V_{in}}{R_1 \parallel R_2} - \frac{v_o}{R_2}$$

Also:
$$i_N = \frac{v_o}{R_{eq}} + C_{eq} \frac{dv_o}{dt}$$

$$\Rightarrow R_2 C_{eq} \frac{dv_o}{dt} + v_o = A_o \cdot V_{in}$$

$$v_o(t) = A_o \cdot V_{in} \left[1 - e^{-\frac{t}{\tau}} \right] \cdot u(t)$$

Example:

Advantages of CFTs

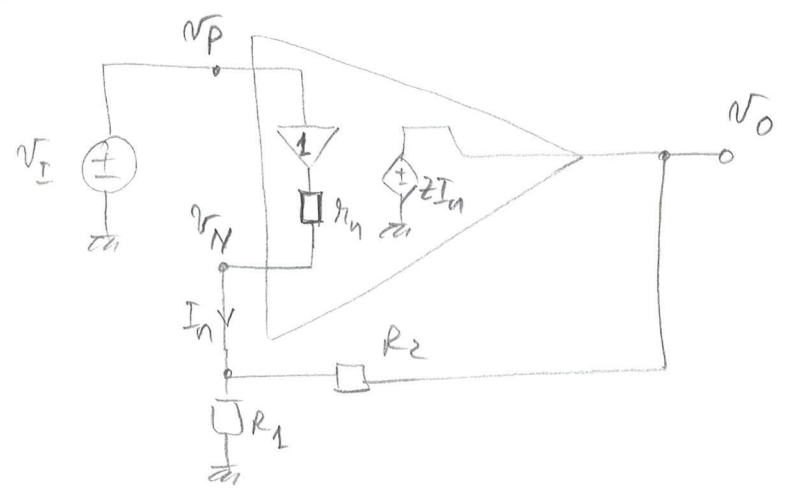
$R_2 = 1.5k \Rightarrow \tau \approx 1ns$ (Contrast to 150ns of $\mu A741$)
 Rise time $t_R = 2.2\tau \approx 2.2ns$ ($t_R = 350ns$ for $\mu A741$)

$$\tau = R_2 C_{eq} \text{ depends on } R_2!$$

Compare to eq. (6.256)

$$\tau = \frac{1}{2\pi f_t} \Rightarrow f_t = \frac{g_{m1}}{2\pi C_e}$$

Second order effects

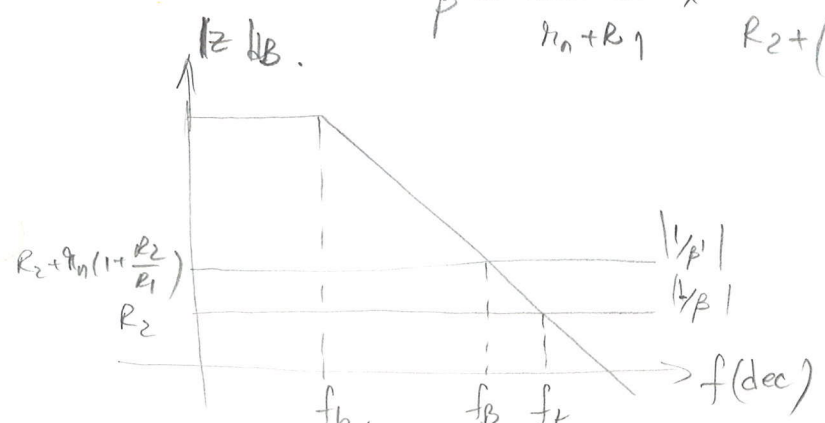


Disadvantages of CFT:

- ⊖ poorer V_{os} , I_{n1} , I_p characteristics!
- ⊖ Noisier because lower bandwidths!
- Suitable for fast but moderately accurate applications

$$I_n = \frac{V_o}{r_n + R_1 \parallel R_2} - \beta V_o$$

$$\beta' = \frac{R_1}{r_n + R_1} \times \frac{1}{R_2 + (r_n \parallel R_1)} = \frac{1}{R_2 + r_n \left(1 + \frac{R_2}{R_1} \right)}$$



Shift $|1/\beta|$ upwards
 \Downarrow
 bandwidth is actually smaller!