

## 5 The natural response using $H(s)$

How to use  $H(s)$  to derive the natural response of a circuit?  
This is the core when there are no applied signals!

$$H(s) = K \frac{(s-z_1)(s-z_2)\dots(s-z_m)}{(s-p_1)(s-p_2)\dots(s-p_n)} = \frac{N(s)}{D(s)}$$

Note: Subtle obs is that all this discussion can be done w/o having Laplace transforms introduced!!! Talk in class about it!

For a circuit to yield a response  $y(t) \neq 0$ :

$$D(s) = 0$$

- The values of  $s$  satisfying this equation are precisely the poles  $p_1, p_2, \dots, p_n$  of  $H(s)$ , indicating that the transfer/network function contains all the information needed to predict the functional form of the natural response! This is the real function:

$$y(t) = A_1 e^{p_1 t} + A_2 e^{p_2 t} + \dots + A_n e^{p_n t}$$

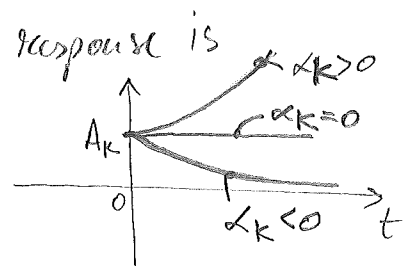
$A_1, A_2, \dots, A_n$ : suitable time-independent coefficients reflecting the initial-conditions in the circuit.

Case 1: Real poles:  $p_k = \alpha_k + j0$

Its contribution to the natural response is

$$y_k(t) = A_k \cdot e^{\alpha_k t}$$

↑ real.

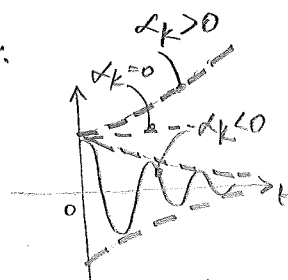


Case 2: Complex pole pairs

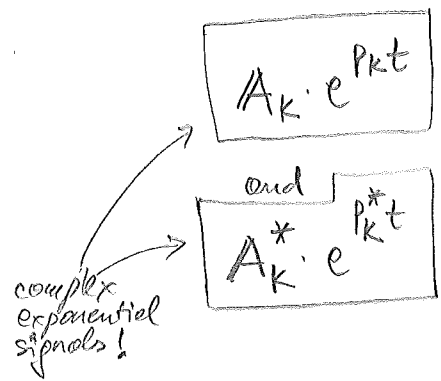
$$p_k = \alpha_k \pm j\omega_k$$

Their combined contribution to the natural response is:

$$y_k(t) = 2|A_k| \cdot e^{\alpha_k t} \cdot \cos(\omega_k t + \theta_k)$$



where:  $A_k = |A_k| \cdot \theta_k$  gives the complex-exponential terms:



that corresponds to  $p_k = \alpha_k + j\omega_k$

that corresponds to  $p_k^* = \alpha_k - j\omega_k$

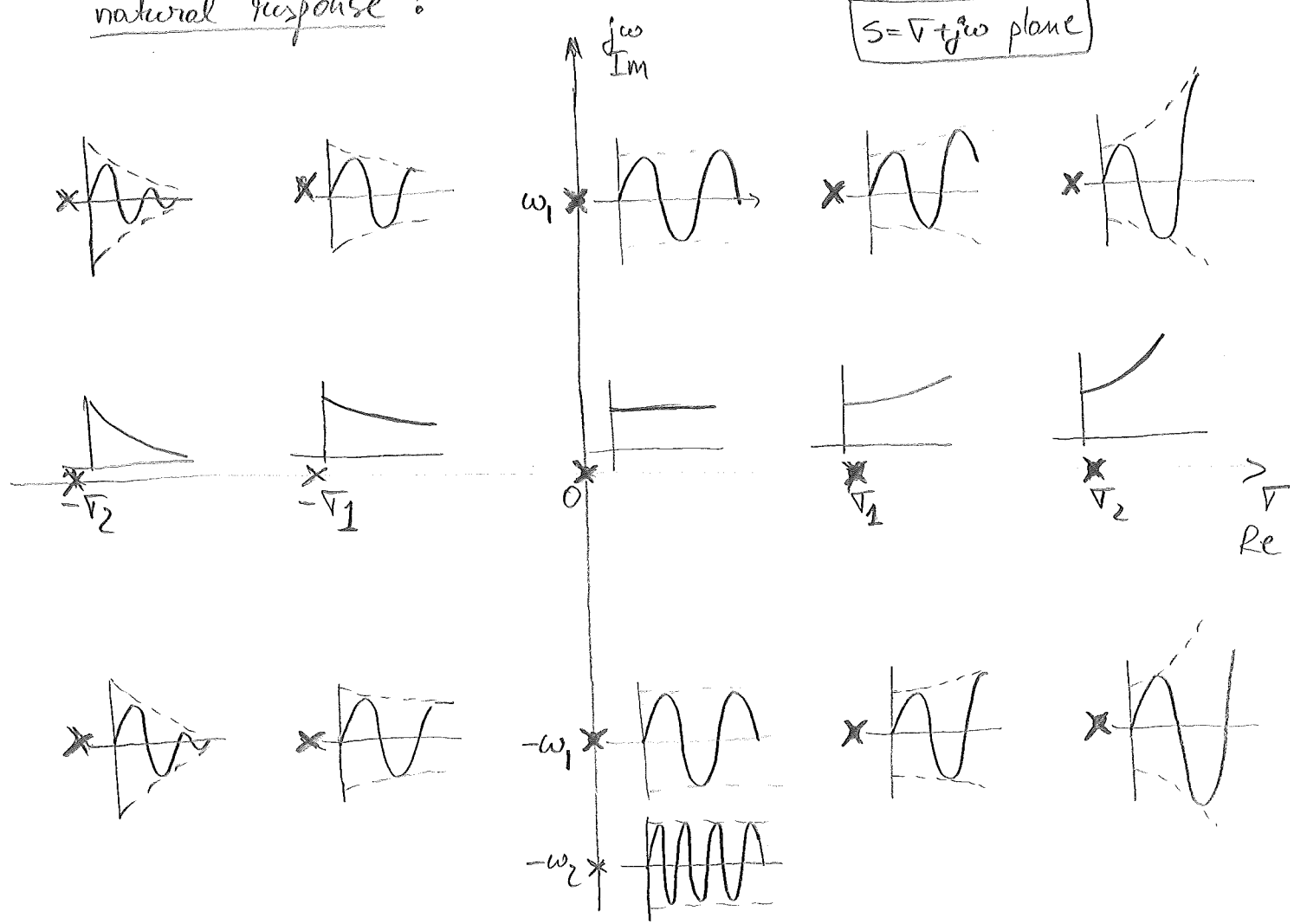
**Case 3** Repeated poles

If Pole  $p_k$  has multiplicity  $n_k$ , then:

$$y_k(t) = [A_{k,0} + A_{k,1}t + A_{k,2}t^2 + \dots + A_{k,n_k-1}t^{n_k-1}] \cdot e^{p_k t}$$

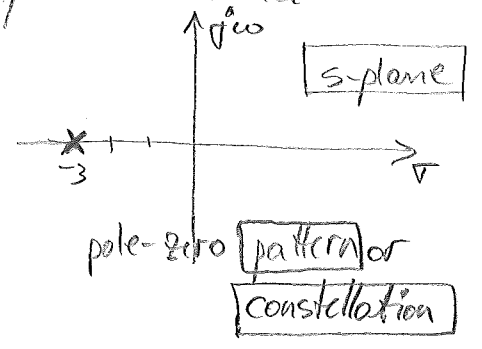
- A visual correspondence between the location of a pole in the  $s$ -plane and the functional form of its contribution to the natural response:

$s = \sigma + j\omega$  plane

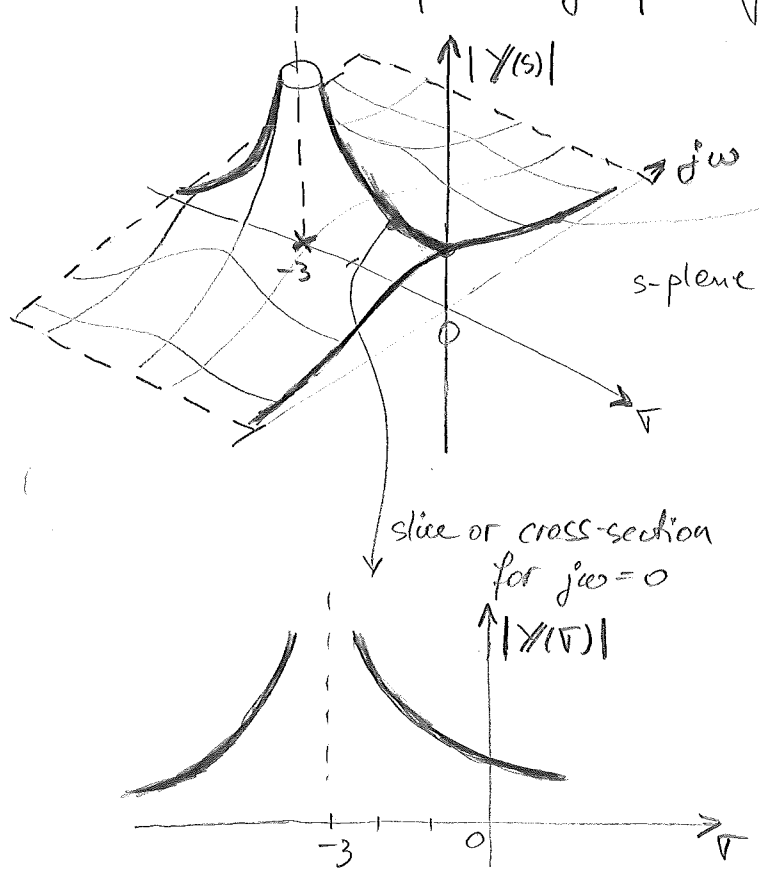


**Example 1:** Sketch the magnitude plot for admittance:

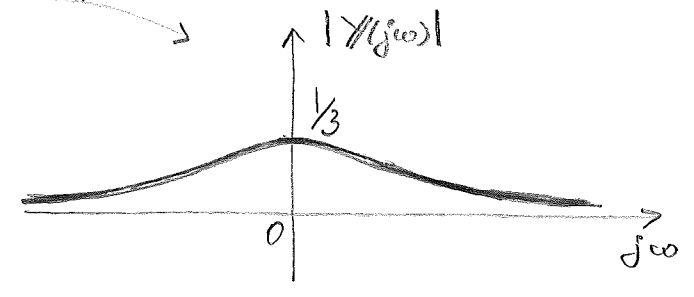
$$Y(s) = \frac{1}{s+3} \leftarrow \text{pole } p_1 = -3$$



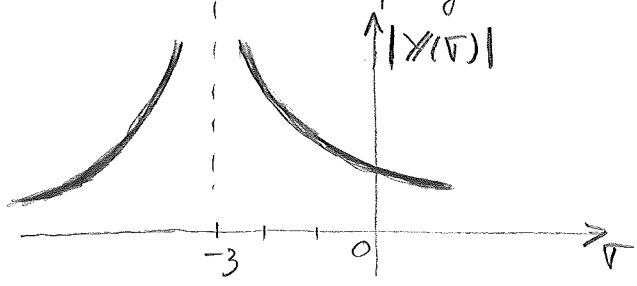
$$|Y(s)| = \left| \frac{1}{\sigma + j\omega + 3} \right| = \frac{1}{|\sigma + 3 + j\omega|} = \frac{1}{\sqrt{(\sigma+3)^2 + \omega^2}}$$



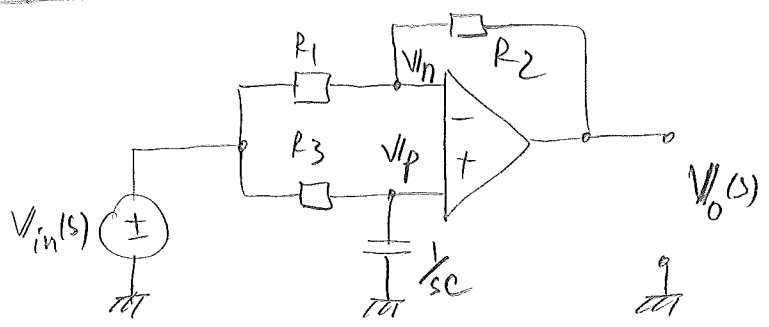
slice or cross-section for  $\sigma = 0$



slice or cross-section for  $j\omega = 0$



**Example 2:** Find the transfer function for the circuit:



$$H(s) = \frac{V_O(s)}{V_{in}(s)} = ?$$

Use superposition:

$$V_o = -\frac{R_2}{R_1} V_{in} + \left(1 + \frac{R_2}{R_1}\right) V_p \quad (1)$$

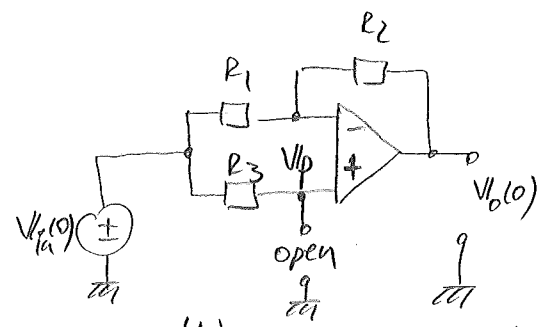
where:  $V_p = \frac{\frac{1}{sC}}{R_3 + \frac{1}{sC}} V_{in} = \frac{1}{R_3Cs + 1} V_{in} \quad (2)$   $\Rightarrow$

$$\Rightarrow H(s) = \frac{V_o(s)}{V_{in}(s)} = \frac{-R_2R_3C \cdot s + R_1}{R_1R_3C \cdot s + R_1}$$

Asymptotic checks

Let  $s \rightarrow 0 \Rightarrow H(0) = 1 \frac{V}{V}$

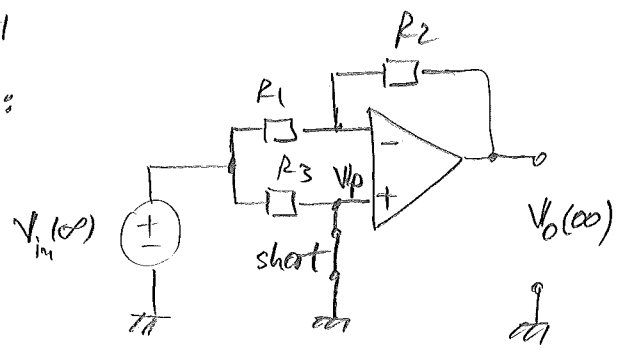
confirmation:



$$V_p = V_{in} \xrightarrow{(1)} V_o = V_{in} \Rightarrow \frac{V_o}{V_{in}} = 1 \quad (!)$$

Let  $s \rightarrow \infty \Rightarrow H(\infty) = -\frac{R_2}{R_1}$

confirmation:



$$V_p = 0 \xrightarrow{(1)} V_o = -\frac{R_2}{R_1} V_{in} \Rightarrow$$

$$\Rightarrow \frac{V_o}{V_{in}} = -\frac{R_2}{R_1} \quad (!)$$

